

Design of Cognitive Receiver RF Front-End Control

Eyosias Yoseph Imana, Jeffery H. Reed (Ph.D)
Wireless@VT, Virginia Tech

Content

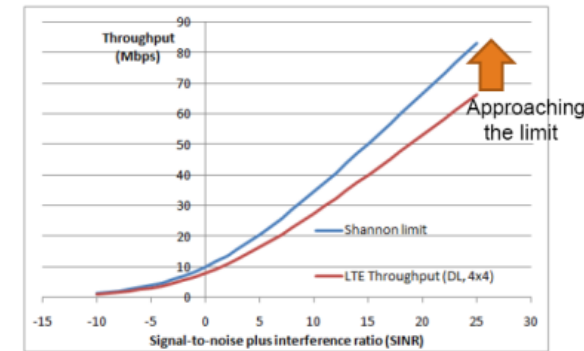
- The (near) future (problem statement)
- Introduction to cognitive control
- Modeling of the spectrum
- Cognitive engine design
- Theoretical analysis
- Conclusion

Content

- The (near) future (problem statement)
- Introduction to cognitive control
- Modeling of the spectrum
- Cognitive engine design
- Theoretical analysis
- Conclusion

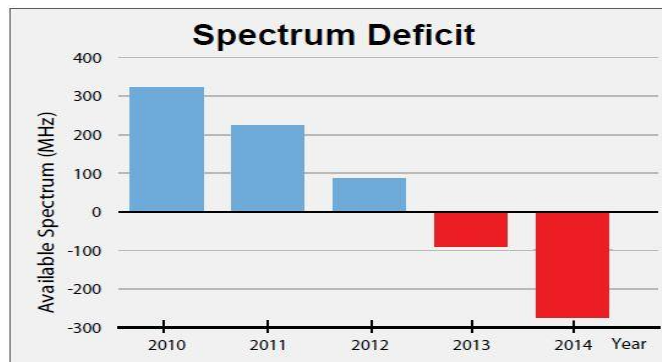
The (Near) Future: The Spectrum

- Already close to the limit to modulation and coding can provide
- Demand is increasing (a looming spectrum deficit)
- Efficient utilization of the spectrum is the remaining knob to increase capacity
 - Note that historical capacity gains come mainly from frequency re-use
- More energetic and unpredictable spectrum is expected
 - Less number of white spaces
 - W per Hz is expected to rise



Rupert Baines, "The Best That LTE Can Be: Why LTE Needs Femtocells"

<http://www.hightechforum.org/spectrum-deficit-disorder/>

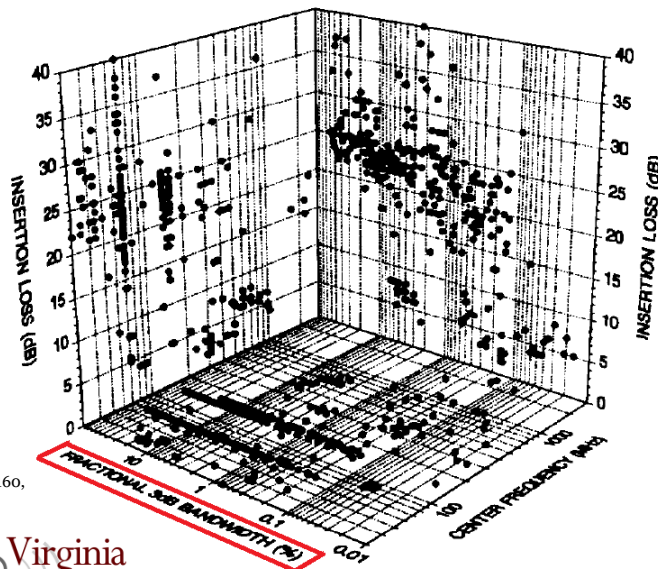


The FCC projects a spectrum deficit by the year 2013



The (Near) Future: The Radio

- Both flexibility and selectivity are on demand
- Technological trade-off
 - Flexible filters are not as selective**

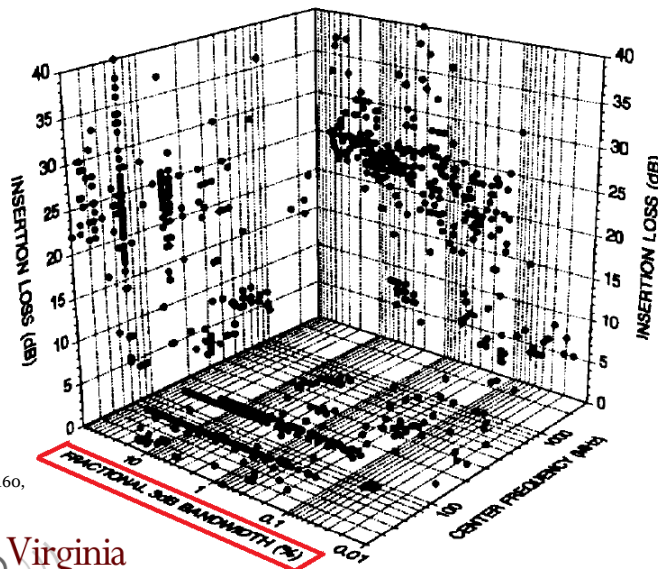


A. Coon, "SAW filters and competitive technologies: a comparative review," *Proceedings of Ultrasonics Symposium, 1991*, pp. 155-160, 1991.

Technology	Frequency Range (GHz)	10-dB BW (%)	Max. IL(dB)	Size
BST	0.49 – 0.79 (1.62:1)	≈ 40	3.0	≈20 cm ²
BST	0.18 – 0.28 (1.56:1)	≈ 50	2.0	≈15 cm ²
BST	0.23 – 0.40 (1.73:1)	≈ 25	2.5	≈ 2 cm ²
Semiconductor	0.70 – 1.33 (1.90:1)	≈ 30	6.0	≈10 cm ²
MEMS	1.50 - 2.50 (1.67:1)	≈ 12	2.2	≈0.5 cm ²
Semiconductor	0.50 – 0.90 (1.80:1)	≈ 28	2.0	0.16 cm ²
Semiconductor	1.40 – 2.00 (1.42:1)	≈ 10	3.0	0.64 cm ²
MEMS	3.55 – 4.71 (1.32:1)	≈ 3	3.55	≈8 cm ²
MEMS	4.30 – 5.50 (1.28:1)	≈ 10	5.3	1.0 cm ³
MEMS	0.70 – 2.26 (3.23:1)	≈ 50	6.0	0.6 cm ²
MEMS (Switch)	1.50 – 2.50 (1.67:1)	≈ 20	8.0	0.7 cm ²
MEMS (Switch)	2.60 - 3.60 (1.37:1)	≈ 15	5.0	0.7 cm ²
MEMS (Switch)	3.70 - 5.40 (1.45:1)	≈ 15	12.5	1.2 cm ²
Semiconductor	0.95 – 1.48 (1.55:1)	≈ 13	4.0	1.87cm ²

The (Near) Future: The Radio

- Both flexibility and selectivity are on demand
- Technological trade-off
 - Flexible filters are not as selective**



A. Coon, "SAW filters and competitive technologies: a comparative review," *Proceedings of Ultrasonics Symposium, 1991*, pp. 155-160, 1991.

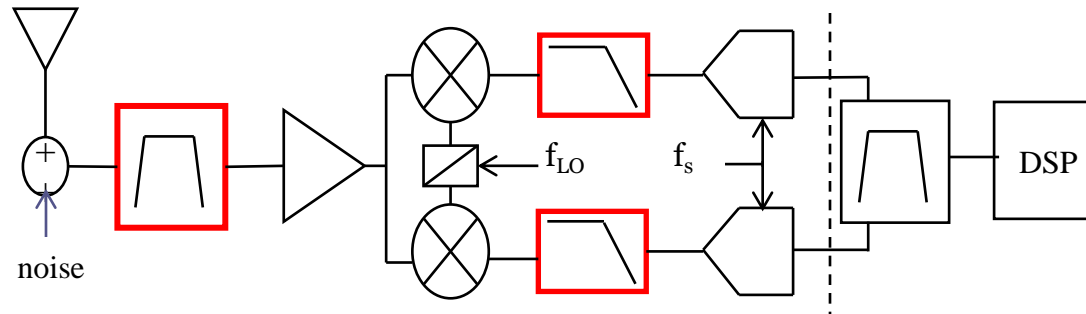
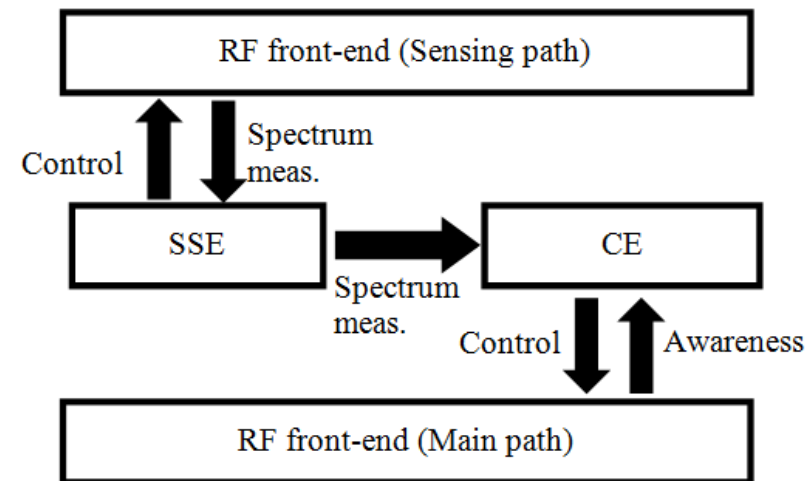
Technology	Frequency Range (GHz)	10-dB BW (%)	Max. IL(dB)	Size
BST	0.49 – 0.79 (1.62:1)	≈ 40	3.0	≈20 cm ²
BST	0.18 – 0.28 (1.56:1)	≈ 50	2.0	≈15 cm ²
BST	0.23 – 0.40 (1.73:1)	≈ 25	2.5	≈ 2 cm ²
Semiconductor	0.70 – 1.33 (1.90:1)	≈ 30	6.0	≈10 cm ²
MEMS	1.50 - 2.50 (1.67:1)	≈ 12	2.2	≈0.5 cm ²
Semiconductor	0.50 – 0.90 (1.80:1)	≈ 28	2.0	0.16 cm ²
Semiconductor	1.40 – 2.00 (1.42:1)	≈ 10	3.0	0.64 cm ²
MEMS	3.55 – 4.71 (1.32:1)	≈ 3	3.55	≈8 cm ²
MEMS	4.30 – 5.50 (1.28:1)	≈ 10	5.3	1.0 cm ³
MEMS	0.70 – 2.26 (3.23:1)	≈ 50	6.0	0.6 cm ²
MEMS (Switch)	1.50 – 2.50 (1.67:1)	≈ 20	8.0	0.7 cm ²
MEMS (Switch)	2.60 - 3.60 (1.37:1)	≈ 15	5.0	0.7 cm ²
MEMS (Switch)	3.70 - 5.40 (1.45:1)	≈ 15	12.5	1.2 cm ²
Semiconductor	0.95 – 1.48 (1.55:1)	≈ 13	4.0	1.87cm ²

Content

- The (near) future (problem statement)
- **Introduction to cognitive control**
- Modeling of the spectrum
- Cognitive engine design
- Theoretical analysis
- Conclusion

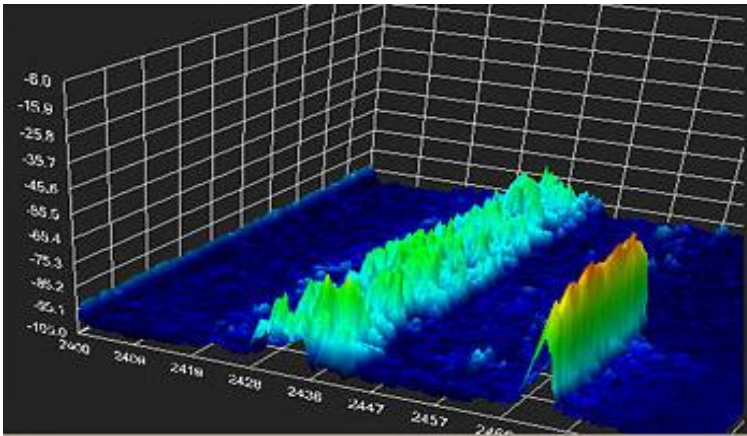
Proposed solution

- Use of cognitive control to reduce selectivity requirements of:
 - Pre-selector filter
 - Image rejection ratio in the mixer
 - Anti-aliasing filter
 - LNA linearity
- This may relax the tradeoff between selectivity and flexibility of RF front-ends
- Sampling frequency and local oscillator frequency are controlled cognitively. The control employs:
 - Cognitive engine (CE)
 - Spectrum sensing engine (SSE)



Features of Proposed Cognitive RF Front-end Control

Sensing



Self-awareness



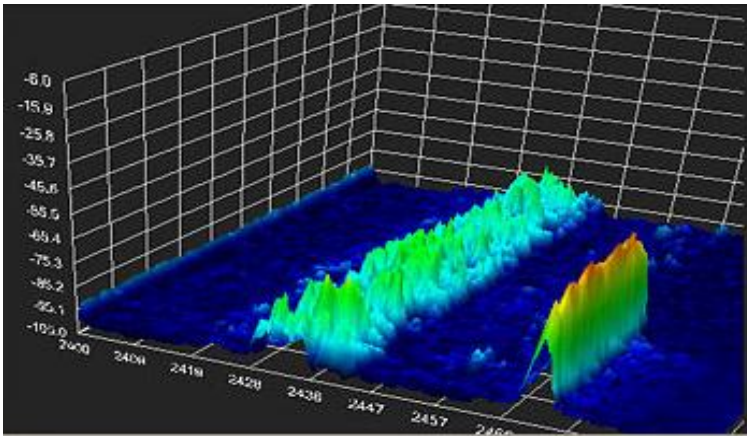
Intelligence



Exploiting experience



Features of Proposed Cognitive RF Front-end Control Sensing



Self-awareness



Intelligence



Exploiting experience

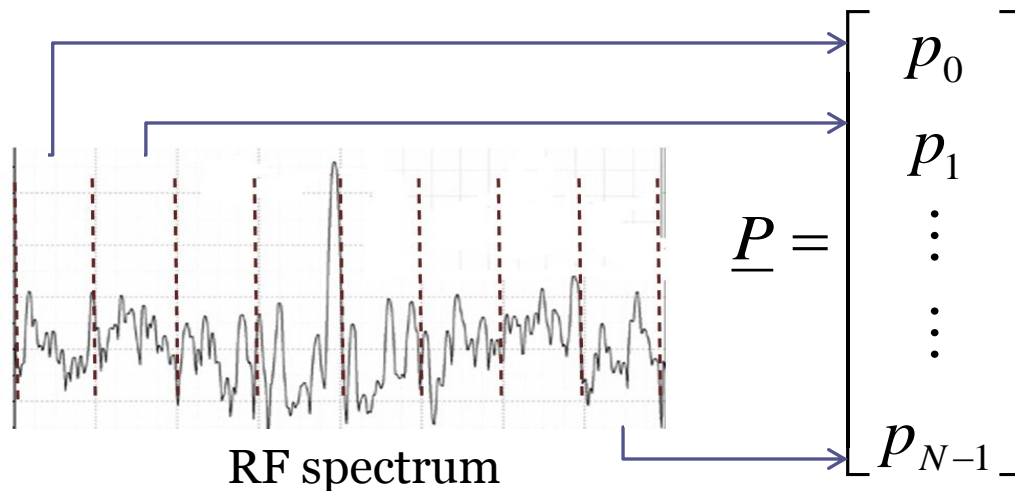


Content

- The (near) future (problem statement)
- Introduction to cognitive control
- **Modeling of the spectrum**
- Cognitive engine design
- Theoretical analysis
- Conclusion

Modeling the Spectrum

- The spectrum is modeled by a vector representing the *power spectrum domain* of the signal
- *Power spectrum domain: Average power* contained in a given sub-band of the spectrum



Note: For time-multiplexed communication systems, we show that each element of \underline{P} follows Pareto distribution

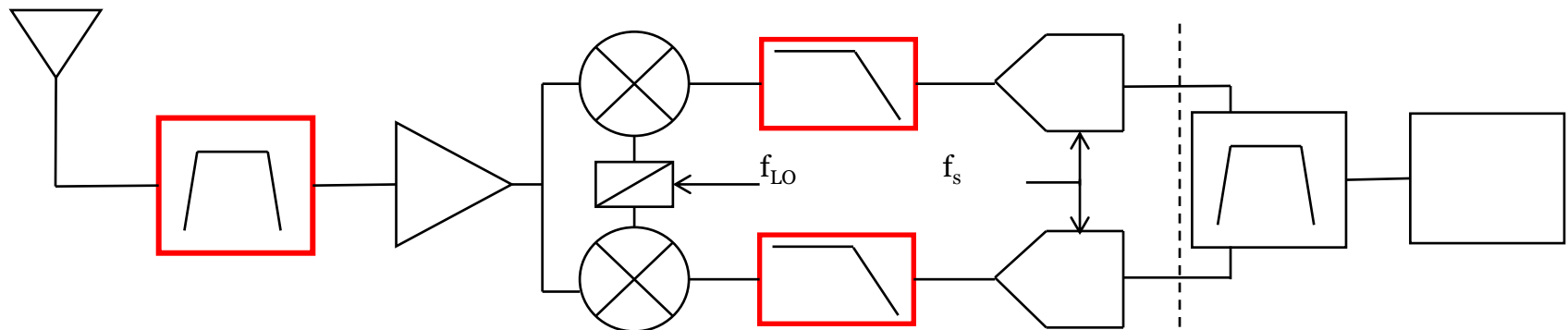
$$f_P(P) = \begin{cases} \left(\frac{P_{min}^{2/n}}{1 - \left(\frac{P_{min}}{P_{TX}} \right)^{2/n}} \right) \frac{2}{nP^{1+\frac{2}{n}}}, & P_{min} \leq P \leq P_{TX} \\ 0, & \text{otherwise} \end{cases}$$

Content

- The (near) future (problem statement)
- Introduction to cognitive control
- Modeling of the spectrum
- **Cognitive engine design**
- Theoretical analysis
- Conclusion

Self-Awareness (1/5)

- Each element of the RF front-end between the mixer and the ADC can be modeled as a matrix in the power spectrum domain
- This is valid under the assumption that signals in each sub-band are uncorrelated to each other



$$\begin{aligned}
 \underline{P} = \begin{bmatrix} p_1 \\ p_2 \\ \vdots \\ \vdots \\ p_M \end{bmatrix} &\xrightarrow{\text{Complex mixer}} \underline{P}^{mix} = \begin{bmatrix} p_{-K}^{mix} \\ p_{-K+1}^{mix} \\ \vdots \\ \vdots \\ p_K^{mix} \end{bmatrix} \xrightarrow{\text{filter}} \underline{P}^{fil} = \begin{bmatrix} p_{-K}^{fil} \\ p_{-K+1}^{fil} \\ \vdots \\ \vdots \\ p_K^{fil} \end{bmatrix} \xrightarrow{\text{sampler}} \underline{P}^{adc} = \begin{bmatrix} p_{-D_{fs}}^{adc} \\ p_{-D_{fs}+1}^{adc} \\ \vdots \\ \vdots \\ p_{D_{fs}}^{adc} \end{bmatrix}
 \end{aligned}$$

Self-Awareness(2/5)

- Mixer: $p^{mix}(k; i_{LO}) = p(k + i_{LO}) + \beta \cdot p(k - i_{LO})$

$$\underline{P}^{mix}(i_{LO}) = \underline{A}^{mix}(i_{LO}) \cdot \underline{P}$$

$$i_{LO} = 1, 2, \dots, M$$

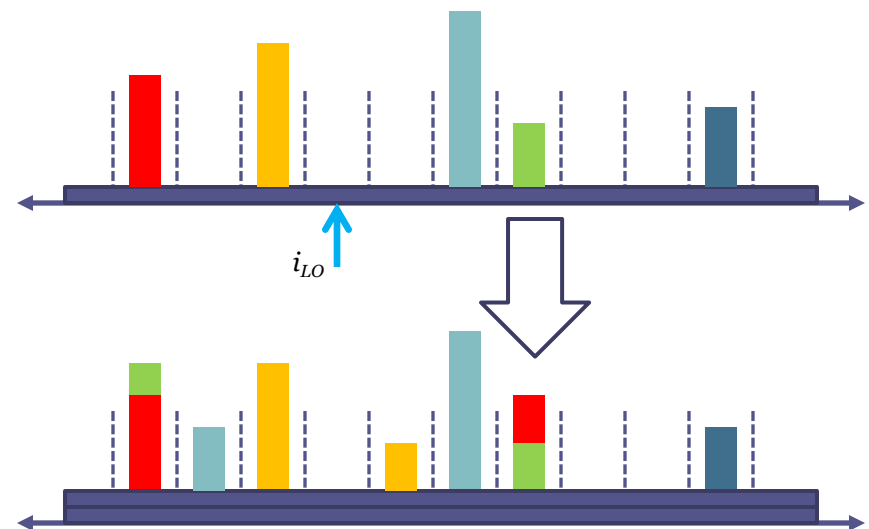
i_{LO} : index of the sub-band containing LO frequency

β : image-rejection ratio of complex mixer

Example:

- $M = 9$
- $i_{LO} = 3$

$$\underline{A}^{mix}(3) = \begin{bmatrix} 1 & 0 & 0 & 0 & 0 & 0 & \beta & 0 & 0 \\ 0 & 1 & 0 & 0 & 0 & \beta & 0 & 0 & 0 \\ 0 & 0 & 1 & 0 & \beta & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 1 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & \beta & 0 & 1 & 0 & 0 & 0 & 0 \\ 0 & \beta & 0 & 0 & 0 & 1 & 0 & 0 & 0 \\ \beta & 0 & 0 & 0 & 0 & 0 & 1 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 1 \end{bmatrix}$$



Self-Awareness(3/5)

- **Filter:** $p^{fil}(l; i_{LO}) = p^{mix}(l; i_{LO}) |H(l)|^2$

H : represents frequency transform of the filter

$$\underline{P}^{fil}(i_{LO}) = \underline{A}^{fil} \cdot \underline{P}^{mix}(i_{LO})$$

Note: Filter is not non-linear. Hence, \underline{A}^{fil} is a diagonal matrix

- **Sampler:** $p^{adc}(d; i_{LO}, l_{fs}) = \sum_{m=-\lfloor (K-d)/l_{fs} \rfloor}^{\lfloor (K+d)/l_{fs} \rfloor} Q_m p^{fil}(d - ml_{fs}; i_{LO})$

Q_m : represents filtering due to non-impulsive sampling

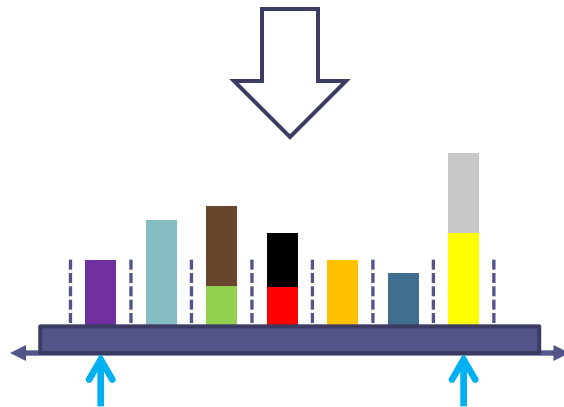
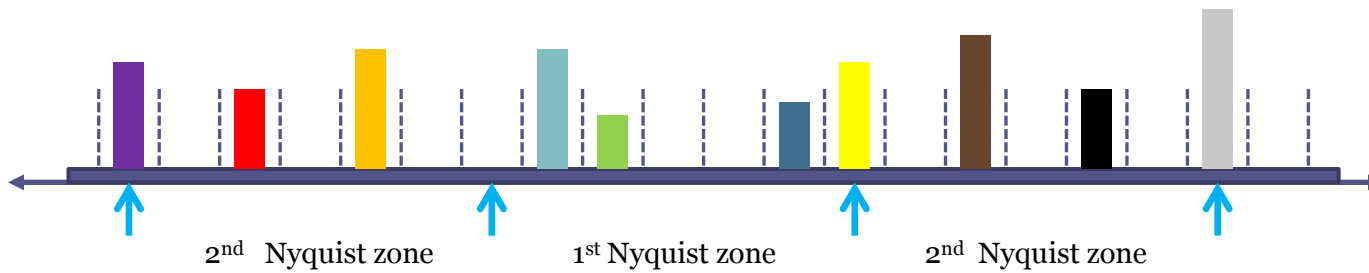
l_{fs} : sub-band containing sampling frequency

$$\underline{P}^{adc}(l_{fs}, i_{LO}) = \underline{A}^{adc}(l_{fs}) \underline{P}^{fil}(i_{LO})$$

Note: Dimensions of \underline{A}^{adc} are dependent on the sampling frequency

Self-Awareness(4/5)

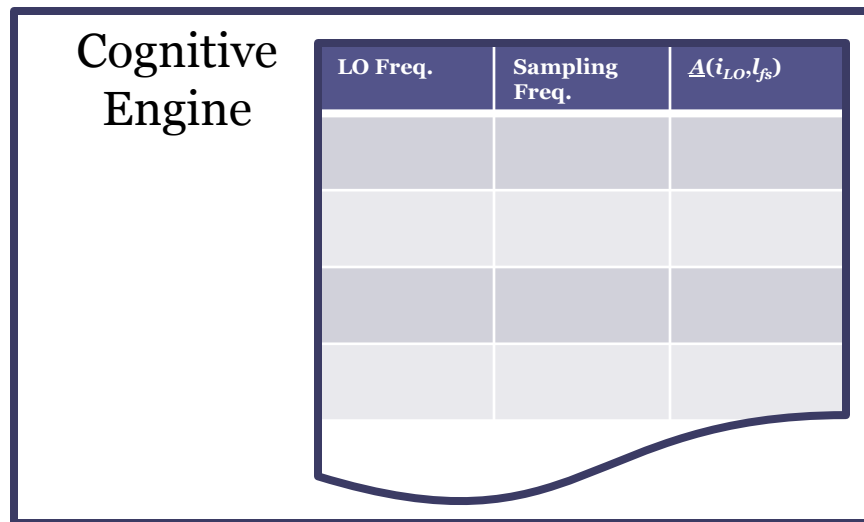
- Example:



$$\underline{A}^{adc}(6) = \begin{bmatrix} Q_1 & 0 & 0 & 0 & 0 & 0 & 1 & 0 & 0 & 0 & 0 & 0 & Q_1 & 0 & 0 & 0 & 0 & 0 & Q_2 & 0 \\ 0 & Q_1 & 0 & 0 & 0 & 0 & 0 & 1 & 0 & 0 & 0 & 0 & 0 & Q_1 & 0 & 0 & 0 & 0 & 0 & Q_2 \\ 0 & 0 & Q_1 & 0 & 0 & 0 & 0 & 0 & 1 & 0 & 0 & 0 & 0 & 0 & Q_1 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & Q_1 & 0 & 0 & 0 & 0 & 0 & 1 & 0 & 0 & 0 & 0 & 0 & Q_1 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & Q_1 & 0 & 0 & 0 & 0 & 0 & 1 & 0 & 0 & 0 & 0 & 0 & Q_1 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & Q_1 & 0 & 0 & 0 & 0 & 0 & 1 & 0 & 0 & 0 & 0 & 0 & Q_1 & 0 & 0 \end{bmatrix}$$

Self-Awareness (5/5)

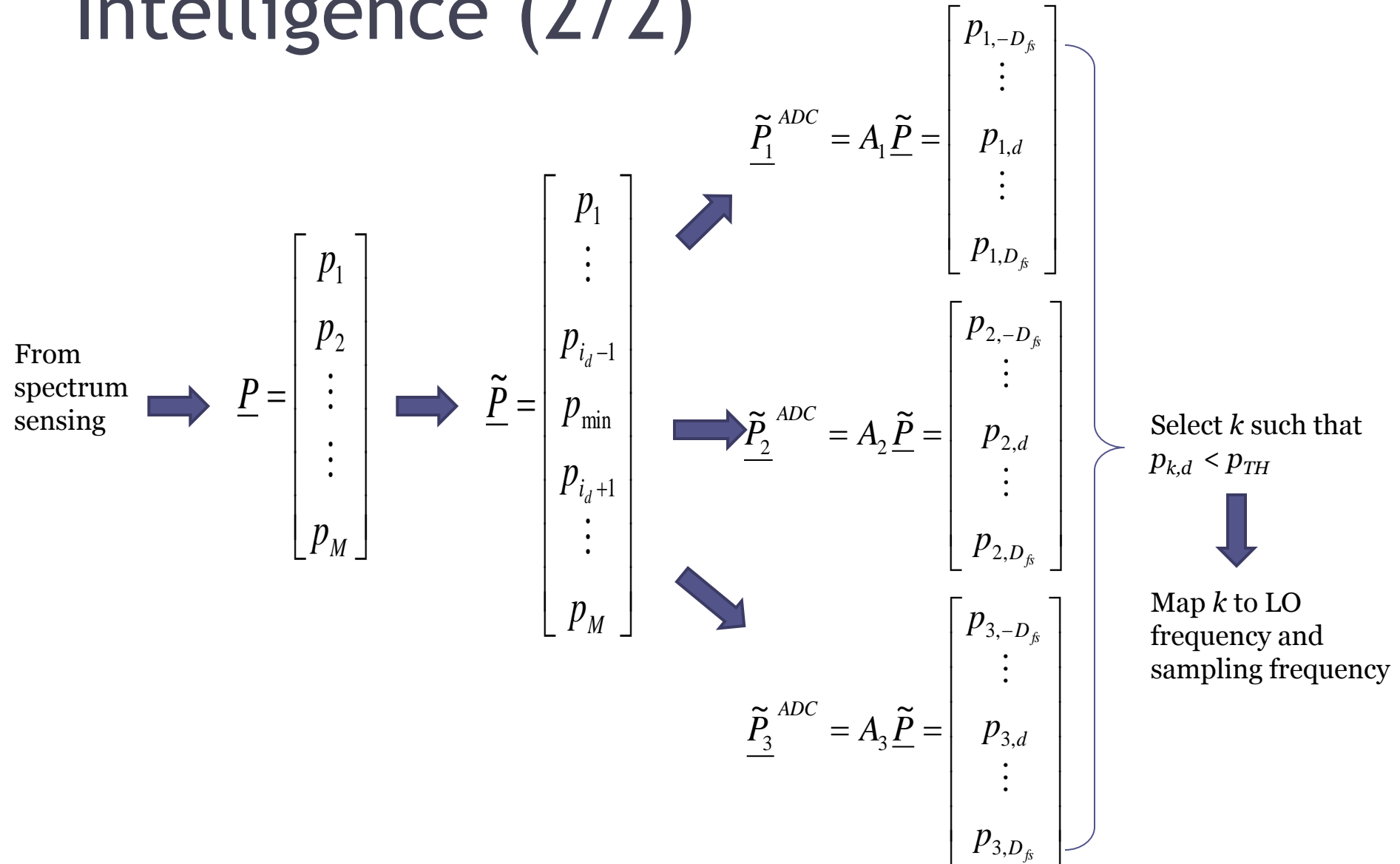
- Model of the RF front-end:
$$\underline{A}(i_{LO}, l_{fs}) = \underline{A}^{mix}(i_{LO}) \cdot \underline{A}^{fil} \cdot \underline{A}^{adc}(l_{fs})$$
$$\underline{P}^{adc}(i_{LO}, l_{fs}) = \underline{A}(i_{LO}, l_{fs}) \cdot \underline{P}$$
- The CE is made “aware” of the RF front-end by storing $\underline{A}(i_{LO}, l_{fs})$ for every possible LO frequency and sampling frequency



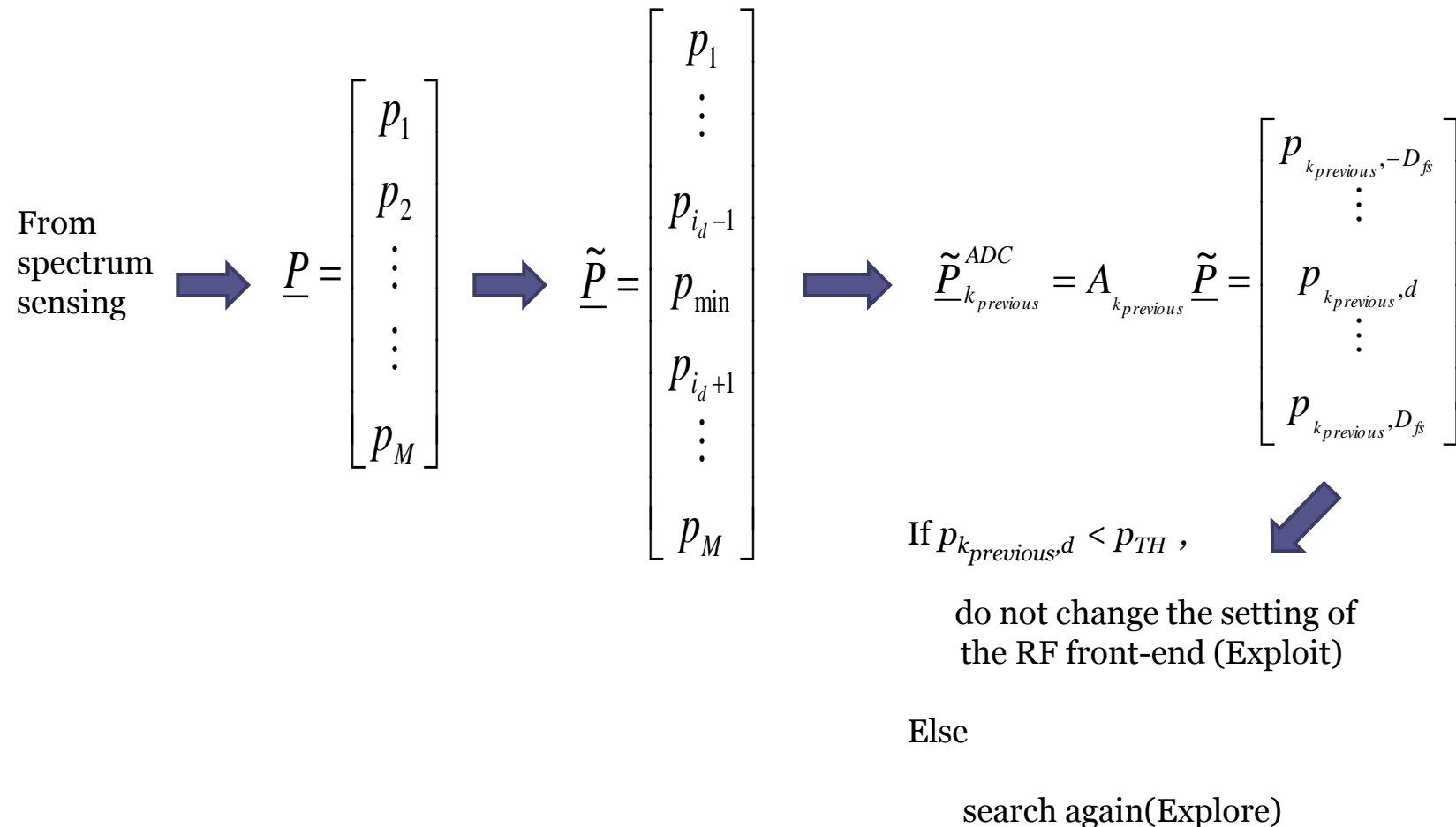
Intelligence (1 / 2)

- The energy content of the overall signal is redistributed as it traverses through the RF front-end
- We propose the use of CE to select a the i_{LO} and l_{fs} which minimize the amount of undesired power that folds into the desired sub-band
- The CE is implemented as a simple search algorithm

Intelligence (2/2)



Exploitation



Content

- The (near) future (problem statement)
- Introduction to cognitive control
- Modeling of the spectrum
- Cognitive engine design
- **Theoretical analysis**
- Conclusion

Theoretical Analysis (1 / 3)

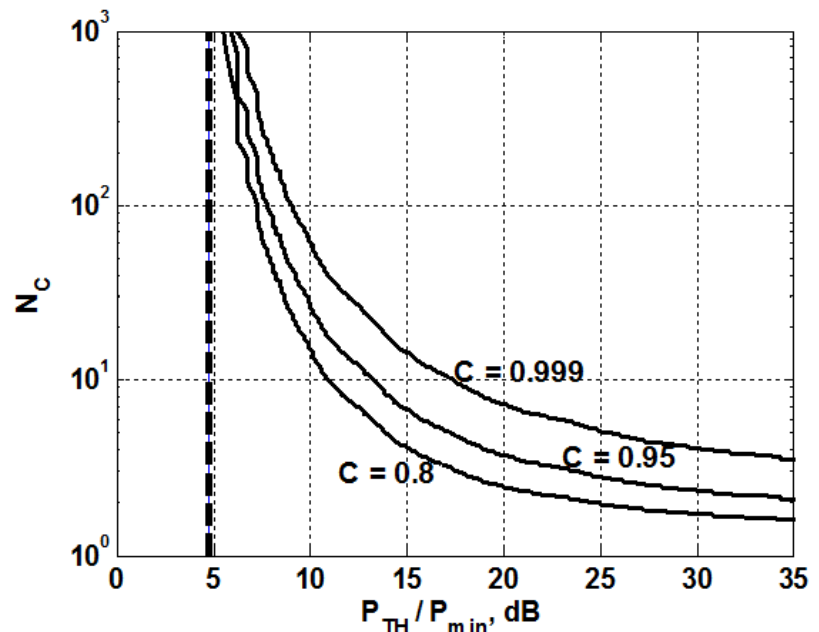
- Feasibility of implementing the CE as a search algorithm was analyzed

$$N_c \approx \frac{\ln(1 - C)}{\ln(1 - p_s(P_{TH}))}$$

N_c : Number of independent trials the CE takes to find a solution with C degree of confidence

C : degree of confidence

$p_s(p_{TH})$: probability that the power of the signal in given sub-band in the spectrum is below p_{TH}

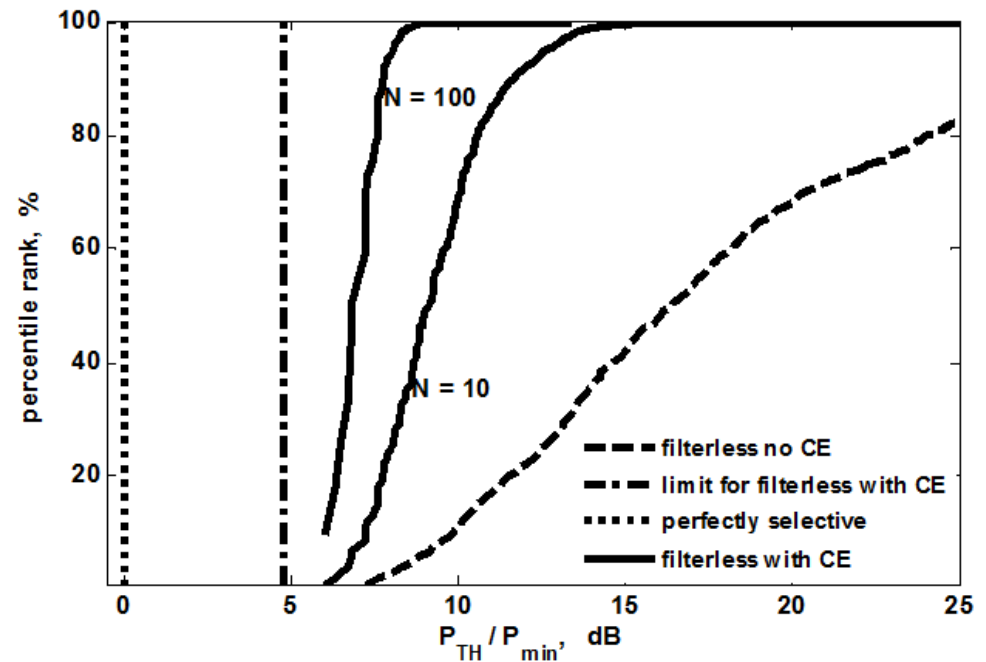


Theoretical Analysis (2/3)

- Comparing the performance of;
 - Perfectly selective RF front-end
 - Filter-less RF front-end
 - Cognitively controlled filter-less RF front-end
- Metric
 - Percentile of the ratio of the undesired power in the desired band with the power of the minimum detectable signal

Theoretical Analysis (3/3)

- Cognitive RF front-end control allows a filter-less RF front-end to behave similar to a highly selective RF front-end



Simulation (1/2)

- RF front-end is operational from 850 MHz to 950 MHz
- Width of each sub-band is 100 kHz
- No pre-selector filter
- 2nd order baseband Butterworth filter
- Maximum possible received power = 30 dBm
- Minimum detectable signal = -100 dBm
- Path-loss exponent = 4
- Probability of occupancy ≈ 0.8
- Sampling frequency varied from 200 kHz to 20 MHz in 200 kHz steps
- LO frequency varied from 900 MHz to 910 MHz in 200 kHz steps
- Simulation was re-run 100 times
- The average number of steps the CE takes to find a solution and the average of the sampling frequencies suggested by the CE are recorded

Simulation (2/2)

P_{TH}/P_{min} (dB)	With exploitation		Without exploitation			Theoretical Approximation
	Average N	Average sampling frequency (MHz)	Average N	Average sampling frequency (MHz)	$N_{0.95}$	
5.5	245	3.4	320	2.8	714	998
6.0	125	1.8	160	1.6	405	374
8.0	55	1.4	160	1.6	235	67
10.0	25	0.6	40	0.5	95	20
15.0	5	0.4	10	0.3	44	6
20.0	1	0.2	1	0.2	3	4
30.0	1	0.2	1	0.2	1	2

- Exploitation reduces number of steps by up to 30% at the expense of sub-optimal sampling frequency
- The theoretical approximation of the number of the CE takes to find its solution is accurate within an order of magnitude
- The CE finds solution in less than 100 steps, even for extreme P_{TH}/P_{min} values

Content

- The (near) future (problem statement)
- Introduction to cognitive control
- Modeling of the spectrum
- Cognitive engine design
- Theoretical analysis
- **Conclusion**

Conclusion

- In statistical sense, cognitive control potentially relaxes the selective specification of the receiver RF front-end
- It is feasible to implement the CE as a simple search algorithm